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# 6β-Methyl-3,20-dioxopregn-4-en-17-yl acetate

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Key indicators: single-crystal X-ray study; T = 296 K; mean  $\sigma$ () = 0.000 Å; R factor = 0.039; wR factor = 0.102; data-to-parameter ratio = 10.3.

The title compound,  $C_{24}H_{34}O_4$ , is a precursor of Megestrol acetate. Ring *A* has a half-chair conformation [*Q* = 0.446 (3) Å,  $\theta$  = 54.6 (4)° and  $\varphi$  = 9.5 (4)°]. Ring *D* adopts a 13 $\beta$ -envelope conformation [*Q* = 0.463 (2) Å and  $\varphi$  = 188.2 (3)°].

#### **Related literature**

For the characterization of related structures, see: Evans & Boeyens (1989). Soriano-Garcia *et al.* (2005). Yousuf *et al.* (2011). For the physiological properties of the title compound, see: Mishell (1996).



#### Experimental

Crystal data C<sub>24</sub>H<sub>34</sub>O<sub>4</sub>

 $M_r = 386.51$ 

Orthorhombic,  $P2_12_12_1^2$  a = 10.0411 (3) Å b = 11.3123 (3) Å c = 18.5549 (7) Å V = 2107.61 (12) Å<sup>3</sup>

Data collection

Rigaku R-AXIS RAPID/ZJUG diffractometer Absorption correction: multi-scan (*ABSCOR*; Higashi, 1995)  $T_{\rm min} = 0.946, T_{\rm max} = 0.975$ 

#### Refinement

 $R[F^2 > 2\sigma(F^2)] = 0.039$   $wR(F^2) = 0.102$  S = 1.002679 reflections

Z = 4Mo K\alpha radiation  $\mu = 0.08 \text{ mm}^{-1}$ T = 296 K $0.56 \times 0.52 \times 0.31 \text{ mm}$ 

20014 measured reflections 2679 independent reflections 2108 reflections with  $I > 2\sigma(I)$  $R_{\text{int}} = 0.035$ 

 $\begin{array}{l} 259 \text{ parameters} \\ \text{H-atom parameters constrained} \\ \Delta \rho_{max} = 0.17 \text{ e } \text{ Å}^{-3} \\ \Delta \rho_{min} = -0.16 \text{ e } \text{ Å}^{-3} \end{array}$ 

Data collection: *PROCESS-AUTO* (Rigaku, 2006); cell refinement: *PROCESS-AUTO*; data reduction: *CrystalStructure* (Rigaku, 2007); program(s) used to solve structure: *SHELXS97* (Sheldrick, 2008); program(s) used to refine structure: *SHELXL97* (Sheldrick, 2008); molecular graphics: *ORTEP-3 for Windows* (Farrugia, 1997); software used to prepare material for publication: *WinGX* (Farrugia, 1999).

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Supplementary data and figures for this paper are available from the IUCr electronic archives (Reference: LD2047).

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## supplementary materials

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### 6β-Methyl-3,20-dioxopregn-4-en-17-yl acetate

#### Longran Chen, Xuefen Liu and Peng Yang

#### Comment

 $6\beta$ -methyl-3,20-dioxopregn-4-ene-17-yl acetate and its derivatives (for example, Megestrol acetate) are important progestines used for the treatment of endomentriosis as well as several other applications (Mishell, 1996).

The structure of the title compound is depicted in Fig.1. Ring A (C1—C5, C10) has a slightly distorted half-chair conformation with Q (total puckering amplitude) = 0.446 (3) Å, theta (azimuthal angle) = 54.6 (4) °,  $\varphi$  (phase angle) = 9.5 (4) °, while ring B (C5—C10) and C (C8,C9, C11—C14) are in chair conformation [ring B: Q = 0.521 (2) Å, theta = 12.7 (2) °,  $\varphi$  = 188.7 (13) °; ring C: Q = 0.564 (2) Å, theta = 2.8 (2) °,  $\varphi$  = 267 (4) °] (Evans & Boeyens, 1989). The five-membered ring D exhibits a 13 $\beta$ -envelope conformation with puckering amplitude Q = 0.463 (2) Å and phase angle= 188.2 (3) °. The crystals are isomorphous to 17alpha-Acetoxy-6-methylene-4-pregnene-3,20-dione (Soriano-Garcia *et al.*, 2005). The crystal structure is also similar to 3alpha-Dimethylamino-20-(*N*-methylacetamido)pregn-5-ene (Yousuf *et al.*, 2011).

#### **Experimental**

The title compound was received from Shanghai Xinhualian Pharmaceutical Co., Ltd. Suitable crystals were obtained by slow evaporation of its ethanol solution at room temperature.

#### Refinement

All H atoms were initially located in a difference Fourier map. The methyl H atoms were then constrained to an ideal geometry with C—H distances of 0.98 Å and  $U_{iso}(H) = 1.5U_{eq}(C)$ , but each group was allowed to rotate freely about its C —C bond. All other H atoms were placed in geometrically idealized positions and constrained to ride on their parent atoms with C—H distances in the range 0.93–0.98 Å and  $U_{iso}(H) = 1.2U_{eq}(C)$ .

#### **Computing details**

Data collection: *PROCESS-AUTO* (Rigaku, 2006); cell refinement: *PROCESS-AUTO* (Rigaku, 2006); data reduction: *CrystalStructure* (Rigaku, 2007); program(s) used to solve structure: *SHELXS97* (Sheldrick, 2008); program(s) used to refine structure: *SHELXL97* (Sheldrick, 2008); molecular graphics: *ORTEP-3 for Windows* (Farrugia, 1997); software used to prepare material for publication: *WinGX* (Farrugia, 1999).



#### Figure 1

The molecular structure of (I) with displacement ellipsoids drawn at the 30% probability level.

#### 6β-Methyl-3,20-dioxopregn-4-en-17-yl acetate

Crystal data

C<sub>24</sub>H<sub>34</sub>O<sub>4</sub>  $M_r = 386.51$ Orthorhombic,  $P2_12_12_1$ Hall symbol: P 2ac 2ab a = 10.0411 (3) Å b = 11.3123 (3) Å c = 18.5549 (7) Å V = 2107.61 (12) Å<sup>3</sup> Z = 4

#### Data collection

Rigaku R-AXIS RAPID/ZJUG
diffractometer
Radiation source: rolling anode
Graphite monochromator
Detector resolution: 10.00 pixels mm <sup>-1</sup>
$\omega$ scans
Absorption correction: multi-scan
(ABSCOR; Higashi, 1995)
$T_{\min} = 0.946, T_{\max} = 0.975$

#### Refinement

Refinement on  $F^2$ Least-squares matrix: full  $R[F^2 > 2\sigma(F^2)] = 0.039$  $wR(F^2) = 0.102$ S = 1.002679 reflections 259 parameters 0 restraints Primary atom site location: structure-invariant direct methods Secondary atom site location: difference Fourier map F(000) = 840  $D_x = 1.218 \text{ Mg m}^{-3}$ Mo K\alpha radiation,  $\lambda = 0.71073 \text{ Å}$ Cell parameters from 14918 reflections  $\theta = 3.0-27.4^{\circ}$   $\mu = 0.08 \text{ mm}^{-1}$  T = 296 KChunk, colorless  $0.56 \times 0.52 \times 0.31 \text{ mm}$ 

20014 measured reflections 2679 independent reflections 2108 reflections with  $I > 2\sigma(I)$  $R_{int} = 0.035$  $\theta_{max} = 27.4^\circ$ ,  $\theta_{min} = 3.0^\circ$  $h = -12 \rightarrow 11$  $k = -14 \rightarrow 14$  $l = -24 \rightarrow 24$ 

Hydrogen site location: inferred from neighbouring sites H-atom parameters constrained  $w = 1/[\sigma^2(F_o^2) + (0.0441P)^2 + 0.5695P]$ where  $P = (F_o^2 + 2F_c^2)/3$  $(\Delta/\sigma)_{max} = 0.001$  $\Delta\rho_{max} = 0.17$  e Å<sup>-3</sup>  $\Delta\rho_{min} = -0.16$  e Å<sup>-3</sup> Extinction correction: *SHELXL97* (Sheldrick, 2008), Fc\*=kFc[1+0.001xFc^2\lambda^3/sin(2\theta)]^{-1/4} Extinction coefficient: 0.0057 (12)

#### Special details

**Geometry**. All e.s.d.'s (except the e.s.d. in the dihedral angle between two l.s. planes) are estimated using the full covariance matrix. The cell e.s.d.'s are taken into account individually in the estimation of e.s.d.'s in distances, angles and torsion angles; correlations between e.s.d.'s in cell parameters are only used when they are defined by crystal symmetry. An approximate (isotropic) treatment of cell e.s.d.'s is used for estimating e.s.d.'s involving l.s. planes.

**Refinement**. Refinement of  $F^2$  against ALL reflections. The weighted *R*-factor *wR* and goodness of fit *S* are based on  $F^2$ , conventional *R*-factors *R* are based on *F*, with *F* set to zero for negative  $F^2$ . The threshold expression of  $F^2 > \sigma(F^2)$  is used only for calculating *R*-factors(gt) *etc.* and is not relevant to the choice of reflections for refinement. *R*-factors based on  $F^2$  are statistically about twice as large as those based on *F*, and *R*- factors based on ALL data will be even larger.

 $U_{\rm iso}*/U_{\rm eq}$ х v Z0.53897 (13) 0.0759(7) 01 0.9284(2)-0.06142(15)O2 0.6725(3)0.92350(17)0.70081 (12) 0.0713 (6) O3 0.49550 (16) 0.66587 (14) 0.65423 (9) 0.0439(4)04 0.3669(2)0.82806 (18) 0.65415 (12) 0.0655 (6) C1 0.8845(3)0.1906(2)0.65614 (14) 0.0475 (6) H1A 0.9083 0.2115 0.7052 0.057\* H1B 0.7889 0.1785 0.6547 0.057\* C2 0.9537(3)0.0745 (2) 0.63640 (16) 0.0572(7)H2A 1.0487 0.0825 0.6445 0.069\* H2B 0.9210 0.0120 0.6676 0.069\* C3 0.9299(3)0.0410(2)0.55974 (17) 0.0533(7)C4 0.9105(3)0.1385(2)0.50972 (15) 0.0499 (6) H4 0.8976 0.1195 0.4615 0.060\* C5 0.9097(2)0.2534(2)0.52737 (13) 0.0407 (5) C6 0.8994(3)0.3438(2)0.46795 (14) 0.0461 (6) 0.055\* H6 0.8611 0.3028 0.4263 C7 0.8027(3)0.4433(2)0.48694 (13) 0.0447 (6) H7A 0.8107 0.5055 0.4512 0.054\* 0.054\* H7B 0.7124 0.4130 0.4848 C8 0.8270(2)0.49588 (19) 0.56153 (12) 0.0368(5)H8 0.044\* 0.9157 0.5320 0.5629 C9 0.39747 (19) 0.61904 (12) 0.0373(5)0.8186(2)Н9 0.7299 0.3622 0.6139 0.045\* C10 0.29462 (19) 0.9205(2)0.60597 (13) 0.0388(5)C11 0.8245(3)0.4476(2)0.69591 (12) 0.0441 (6) H11A 0.8099 0.3838 0.7299 0.053\* H11B 0.9129 0.4791 0.7045 0.053\* C12 0.7216(3)0.5454(2)0.71000 (13) 0.0443(6)H12A 0.6327 0.5120 0.7083 0.053\* H12B 0.7354 0.5779 0.7578 0.053\* C13 0.7333(2)0.64437 (19) 0.65394 (13) 0.0362(5)C14 0.7224(2)0.58932 (19) 0.57819 (12) 0.0360(5)0.043\* H14 0.6363 0.5487 0.5768 C15 0.7092(3)0.69619 (19) 0.52808 (13) 0.0436 (6) 0.052\* H15A 0.6611 0.6753 0.4846 H15B 0.7961 0.5149 0.052\* 0.7267 C16 0.6308(3)0.7875(2)0.57264 (13) 0.0441 (6)

Fractional atomic coordinates and isotropic or equivalent isotropic displacement parameters  $(Å^2)$ 

H16A	0.5437	0.8007	0.5515	0.053*
H16B	0.6782	0.8622	0.5740	0.053*
C17	0.6167 (2)	0.7366 (2)	0.64927 (13)	0.0393 (5)
C22	1.0348 (3)	0.3910 (3)	0.44369 (17)	0.0646 (8)
H18A	1.0727	0.4386	0.4814	0.097*
H18B	1.0237	0.4383	0.4011	0.097*
H18C	1.0931	0.3260	0.4334	0.097*
C19	1.0656 (2)	0.3338 (2)	0.62124 (16)	0.0507 (6)
H19A	1.0760	0.3491	0.6718	0.076*
H19B	1.0848	0.4045	0.5945	0.076*
H19C	1.1257	0.2723	0.6068	0.076*
C18	0.8651 (3)	0.7121 (2)	0.66410 (15)	0.0493 (6)
H20A	0.8674	0.7463	0.7114	0.074*
H20B	0.8715	0.7735	0.6286	0.074*
H20C	0.9386	0.6585	0.6586	0.074*
C20	0.6198 (3)	0.8284 (2)	0.70979 (15)	0.0507 (6)
C21	0.5662 (4)	0.7928 (3)	0.78251 (15)	0.0689 (9)
H22A	0.6221	0.8248	0.8197	0.103*
H22B	0.5651	0.7081	0.7861	0.103*
H22C	0.4773	0.8227	0.7880	0.103*
C23	0.3771 (3)	0.7220 (3)	0.65162 (15)	0.0502 (6)
C24	0.2663 (3)	0.6356 (3)	0.6461 (2)	0.0717 (9)
H24A	0.1828	0.6766	0.6486	0.108*
H24B	0.2722	0.5800	0.6851	0.108*
H24C	0.2724	0.5943	0.6010	0.108*

Atomic displacement parameters  $(Å^2)$ 

	$U^{11}$	$U^{22}$	U <sup>33</sup>	$U^{12}$	$U^{13}$	$U^{23}$
01	0.0979 (17)	0.0353 (10)	0.0944 (16)	-0.0064 (10)	0.0245 (14)	-0.0033 (10)
O2	0.0876 (16)	0.0496 (11)	0.0766 (14)	-0.0048 (11)	0.0016 (13)	-0.0149 (10)
03	0.0355 (9)	0.0459 (9)	0.0503 (9)	0.0016 (7)	0.0036 (8)	0.0031 (8)
O4	0.0601 (12)	0.0629 (12)	0.0734 (13)	0.0205 (10)	0.0049 (12)	0.0007 (11)
C1	0.0506 (14)	0.0424 (12)	0.0495 (14)	0.0014 (11)	0.0012 (13)	0.0087 (11)
C2	0.0604 (17)	0.0420 (13)	0.0692 (19)	0.0045 (12)	0.0028 (14)	0.0098 (13)
C3	0.0484 (15)	0.0385 (13)	0.0729 (19)	-0.0019 (11)	0.0133 (14)	0.0025 (13)
C4	0.0523 (16)	0.0423 (13)	0.0552 (15)	-0.0034 (11)	0.0058 (13)	-0.0045 (11)
C5	0.0352 (13)	0.0393 (11)	0.0474 (13)	-0.0006 (10)	0.0043 (11)	0.0000 (10)
C6	0.0541 (15)	0.0419 (12)	0.0424 (13)	0.0001 (11)	0.0059 (12)	-0.0013 (10)
C7	0.0543 (15)	0.0425 (12)	0.0373 (12)	0.0042 (12)	0.0007 (11)	0.0025 (10)
C8	0.0384 (12)	0.0354 (11)	0.0365 (12)	-0.0014 (9)	0.0027 (10)	0.0020 (9)
C9	0.0364 (12)	0.0365 (11)	0.0389 (12)	-0.0004 (9)	0.0011 (10)	0.0024 (9)
C10	0.0379 (13)	0.0354 (11)	0.0432 (13)	-0.0005 (10)	0.0006 (10)	0.0024 (10)
C11	0.0502 (14)	0.0445 (13)	0.0377 (12)	0.0076 (11)	0.0003 (11)	0.0037 (10)
C12	0.0511 (15)	0.0468 (13)	0.0350 (12)	0.0062 (11)	0.0044 (11)	0.0055 (10)
C13	0.0370 (12)	0.0376 (11)	0.0341 (11)	0.0020 (9)	0.0009 (10)	0.0020 (9)
C14	0.0389 (12)	0.0350 (11)	0.0341 (12)	-0.0006 (9)	-0.0001 (10)	0.0038 (9)
C15	0.0525 (14)	0.0392 (12)	0.0390 (12)	0.0024 (11)	0.0031 (11)	0.0067 (10)
C16	0.0476 (14)	0.0396 (12)	0.0452 (13)	0.0045 (11)	0.0028 (11)	0.0075 (10)
C17	0.0389 (12)	0.0382 (11)	0.0407 (12)	-0.0004 (10)	0.0004 (11)	-0.0006 (10)

## supplementary materials

C22	0.070 (2)	0.0561 (16)	0.0677 (19)	0.0004 (14)	0.0255 (16)	0.0074 (15)
C19	0.0370 (13)	0.0499 (14)	0.0651 (17)	0.0009 (11)	-0.0039 (12)	-0.0018 (13)
C18	0.0437 (14)	0.0479 (13)	0.0563 (16)	-0.0037 (11)	-0.0046 (12)	-0.0065 (12)
C20	0.0540 (15)	0.0480 (14)	0.0502 (15)	0.0101 (13)	-0.0013 (13)	-0.0058 (12)
C21	0.087 (2)	0.074 (2)	0.0448 (16)	0.0202 (18)	0.0032 (16)	-0.0082 (14)
C23	0.0421 (14)	0.0628 (17)	0.0457 (14)	0.0108 (12)	0.0045 (12)	0.0053 (13)
C24	0.0409 (15)	0.088 (2)	0.086 (2)	-0.0019 (15)	0.0033 (16)	0.0111 (19)

Geometric parameters (Å, °)

01—C3	1.221 (3)	C12—C13	1.533 (3)
O2—C20	1.210 (3)	C12—H12A	0.9700
O3—C23	1.348 (3)	C12—H12B	0.9700
O3—C17	1.459 (3)	C13—C18	1.540 (3)
O4—C23	1.205 (3)	C13—C14	1.541 (3)
C1—C2	1.530 (3)	C13—C17	1.571 (3)
C1—C10	1.544 (3)	C14—C15	1.531 (3)
C1—H1A	0.9700	C14—H14	0.9800
C1—H1B	0.9700	C15—C16	1.539 (3)
C2—C3	1.491 (4)	C15—H15A	0.9700
C2—H2A	0.9700	C15—H15B	0.9700
C2—H2B	0.9700	C16—C17	1.540 (3)
C3—C4	1.455 (4)	C16—H16A	0.9700
C4—C5	1.341 (3)	C16—H16B	0.9700
C4—H4	0.9300	C17—C20	1.530 (3)
C5—C6	1.508 (3)	C22—H18A	0.9600
C5-C10	1.535 (3)	C22—H18B	0.9600
C6—C7	1.527 (3)	C22—H18C	0.9600
C6—C22	1.529 (4)	C19—H19A	0.9600
С6—Н6	0.9800	C19—H19B	0.9600
C7—C8	1.526 (3)	С19—Н19С	0.9600
С7—Н7А	0.9700	C18—H20A	0.9600
С7—Н7В	0.9700	C18—H20B	0.9600
C8—C14	1.522 (3)	C18—H20C	0.9600
C8—C9	1.544 (3)	C20—C21	1.508 (4)
C8—H8	0.9800	C21—H22A	0.9600
C9—C11	1.536 (3)	C21—H22B	0.9600
C9—C10	1.568 (3)	C21—H22C	0.9600
С9—Н9	0.9800	C23—C24	1.485 (4)
C10—C19	1.549 (3)	C24—H24A	0.9600
C11—C12	1.536 (3)	C24—H24B	0.9600
C11—H11A	0.9700	C24—H24C	0.9600
C11—H11B	0.9700		
C23—O3—C17	118.33 (17)	C12—C13—C14	108.56 (18)
C2-C1-C10	113.8 (2)	C18—C13—C14	111.9 (2)
C2—C1—H1A	108.8	C12—C13—C17	117.73 (19)
C10—C1—H1A	108.8	C18—C13—C17	108.48 (18)
C2—C1—H1B	108.8	C14—C13—C17	99.50 (18)
C10-C1-H1B	108.8	C8—C14—C15	119.02 (19)

	107.7	C8 C14 C12	114.65(10)
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	107.7 112.0(2)	$C_{15} = C_{14} = C_{13}$	114.05(19) 103.05(17)
$C_3 = C_2 = C_1$	112.0 (2)	$C_{13} - C_{14} - C_{13}$	105.95 (17)
$C_{3}$	109.2	$C_{0} = C_{14} = 1114$	100.1
$C_1 = C_2 = H_2 R$	109.2	$C_{13}$ $C_{14}$ $H_{14}$	100.1
$C_3 = C_2 = H_2 B$	109.2	C13 - C14 - H14	100.1
C1 - C2 - H2B	109.2	C14 - C15 - C16	104.30 (18)
$H_2A = C_2 = H_2B$	107.9	CIG CIS HISA	110.9
01 - 03 - 04	121.1 (3)	CI6—CI5—HI5A	110.9
$01 - C_3 - C_2$	123.0 (3)	CI4—CI5—HI5B	110.9
C4—C3—C2	115.9 (2)	С16—С15—Н15В	110.9
C5—C4—C3	125.5 (3)	HI5A—CI5—HI5B	108.9
C5—C4—H4	117.3	C15—C16—C17	106.98 (18)
C3—C4—H4	117.3	C15—C16—H16A	110.3
C4—C5—C6	118.7 (2)	C17—C16—H16A	110.3
C4—C5—C10	121.7 (2)	C15—C16—H16B	110.3
C6—C5—C10	119.59 (19)	C17—C16—H16B	110.3
C5—C6—C7	112.0 (2)	H16A—C16—H16B	108.6
C5—C6—C22	113.0 (2)	O3—C17—C20	110.0 (2)
C7—C6—C22	112.1 (2)	O3—C17—C16	109.87 (19)
С5—С6—Н6	106.4	C20—C17—C16	114.95 (19)
С7—С6—Н6	106.4	O3—C17—C13	104.72 (16)
С22—С6—Н6	106.4	C20—C17—C13	113.3 (2)
C8—C7—C6	113.3 (2)	C16—C17—C13	103.33 (19)
С8—С7—Н7А	108.9	C6—C22—H18A	109.5
С6—С7—Н7А	108.9	C6—C22—H18B	109.5
С8—С7—Н7В	108.9	H18A—C22—H18B	109.5
С6—С7—Н7В	108.9	C6—C22—H18C	109.5
H7A - C7 - H7B	107.7	H18A - C22 - H18C	109.5
C14 - C8 - C7	110.18 (19)	H18B—C22—H18C	109.5
C14 - C8 - C9	108 82 (18)	C10-C19-H19A	109.5
C7 - C8 - C9	109.70 (18)	C10-C19-H19B	109.5
$C_{14}$ $C_{8}$ H8	109.70 (10)	H19A - C19 - H19B	109.5
C7 C8 H8	109.4	C10 C19 H19C	109.5
$C_{1} = C_{2} = H_{2}$	109.4		109.5
$C_{2} = C_{3} = 118$	109.4	H10P C10 H10C	109.5
C11 - C9 - C8	111.91(10) 112.11(10)	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	109.5
CII = C9 = CI0	113.11 (19)	C12 - C18 - H20A	109.5
$C_{8} - C_{9} - C_{10}$	115.10 (18)	C13-C18-H20B	109.5
СП—С9—Н9	106.0	H20A—C18—H20B	109.5
C8—C9—H9	106.0	C13—C18—H20C	109.5
С10—С9—Н9	106.0	H20A—C18—H20C	109.5
C5—C10—C1	108.96 (19)	H20B—C18—H20C	109.5
C5—C10—C19	109.1 (2)	O2—C20—C21	121.1 (3)
C1—C10—C19	109.2 (2)	O2—C20—C17	120.7 (2)
C5—C10—C9	109.04 (19)	C21—C20—C17	117.9 (2)
C1—C10—C9	108.65 (19)	C20—C21—H22A	109.5
C19—C10—C9	111.90 (19)	C20—C21—H22B	109.5
C12—C11—C9	113.5 (2)	H22A—C21—H22B	109.5
C12—C11—H11A	108.9	C20—C21—H22C	109.5
C9—C11—H11A	108.9	H22A—C21—H22C	109.5

C12—C11—H11B	108.9	H22B—C21—H22C	109.5
C9—C11—H11B	108.9	O4—C23—O3	122.9 (3)
H11A—C11—H11B	107.7	O4—C23—C24	126.4 (3)
C13—C12—C11	111.03 (19)	O3—C23—C24	110.7 (2)
C13—C12—H12A	109.4	C23—C24—H24A	109.5
C11—C12—H12A	109.4	C23—C24—H24B	109.5
C13—C12—H12B	109.4	H24A—C24—H24B	109.5
C11—C12—H12B	109.4	C23—C24—H24C	109.5
H12A—C12—H12B	108.0	H24A—C24—H24C	109.5
C12—C13—C18	110.2 (2)	H24B—C24—H24C	109.5
C10—C1—C2—C3	-54.3 (3)	C11—C12—C13—C14	54.6 (3)
C1-C2-C3-O1	-151.0 (3)	C11—C12—C13—C17	166.5 (2)
C1—C2—C3—C4	30.0 (3)	C7—C8—C14—C15	-58.9 (3)
O1—C3—C4—C5	179.6 (3)	C9—C8—C14—C15	-179.2 (2)
C2—C3—C4—C5	-1.4 (4)	C7—C8—C14—C13	177.23 (19)
C3—C4—C5—C6	175.1 (2)	C9—C8—C14—C13	56.9 (2)
C3-C4-C5-C10	-4.2 (4)	C12—C13—C14—C8	-58.6 (2)
C4—C5—C6—C7	137.0 (3)	C18—C13—C14—C8	63.3 (2)
C10—C5—C6—C7	-43.6 (3)	C17—C13—C14—C8	177.79 (18)
C4—C5—C6—C22	-95.2 (3)	C12—C13—C14—C15	169.82 (19)
C10—C5—C6—C22	84.1 (3)	C18—C13—C14—C15	-68.3 (2)
C5—C6—C7—C8	49.1 (3)	C17—C13—C14—C15	46.2 (2)
C22—C6—C7—C8	-79.2 (3)	C8—C14—C15—C16	-162.4 (2)
C6—C7—C8—C14	-176.85 (19)	C13—C14—C15—C16	-33.4 (2)
C6—C7—C8—C9	-57.1 (3)	C14—C15—C16—C17	6.7 (3)
C14—C8—C9—C11	-52.1 (3)	C23—O3—C17—C20	58.0 (3)
C7—C8—C9—C11	-172.7(2)	C23—O3—C17—C16	-69.5 (2)
C14—C8—C9—C10	178.72 (19)	C23—O3—C17—C13	-179.9(2)
C7—C8—C9—C10	58.1 (3)	C15—C16—C17—O3	-89.6 (2)
C4—C5—C10—C1	-18.7(3)	C15—C16—C17—C20	145.7 (2)
C6—C5—C10—C1	161.9 (2)	C15—C16—C17—C13	21.8 (2)
C4—C5—C10—C19	100.4 (3)	C12—C13—C17—O3	-43.0 (3)
C6—C5—C10—C19	-79.0(3)	C18—C13—C17—O3	-169.06 (19)
C4-C5-C10-C9	-137.2(2)	$C_{14} - C_{13} - C_{17} - O_{3}$	73.86 (19)
C6-C5-C10-C9	43.5 (3)	C12—C13—C17—C20	76.9 (3)
C2-C1-C10-C5	47.2 (3)	C18—C13—C17—C20	-49.1 (3)
$C_{2}$ $C_{1}$ $C_{10}$ $C_{19}$	-71.8(3)	$C_{14}$ $C_{13}$ $C_{17}$ $C_{20}$	-166.2(2)
$C_{2}$ $C_{1}$ $C_{10}$ $C_{9}$	165.9 (2)	$C_{12}$ $C_{13}$ $C_{17}$ $C_{16}$	-1581(2)
$C_{11} - C_{9} - C_{10} - C_{5}$	-1783(2)	C18 - C13 - C17 - C16	75 9 (2)
C8-C9-C10-C5	-49.8(2)	$C_{14}$ $C_{13}$ $C_{17}$ $C_{16}$	-412(2)
$C_{11} - C_{9} - C_{10} - C_{10}$	63 1 (3)	03-C17-C20-O2	-1481(3)
C8-C9-C10-C1	-1684(2)	$C_{16} - C_{17} - C_{20} - O_{2}$	-234(4)
$C_{11} - C_{9} - C_{10} - C_{19}$	-575(3)	$C_{13}$ $C_{17}$ $C_{20}$ $C$	95.1 (3)
C8-C9-C10-C19	710(3)	03-C17-C20-C21	37 2 (3)
C8-C9-C11-C12	52.9(3)	$C_{16}$ $C_{17}$ $C_{20}$ $C_{21}$	161.9 (3)
C10-C9-C11-C12	-177 95 (19)	$C_{13}$ $C_{17}$ $C_{20}$ $C_{21}$ $C_{13}$ $C_{17}$ $C_{20}$ $C_{21}$	-796(3)
C9-C11-C12-C13	-54 2 (3)	C17 - 03 - C23 - 04	-92(4)
$C_{11} - C_{12} - C_{13} - C_{18}$	-684(2)	C17 - 03 - C23 - C24	171 3 (2)
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